

Wetting of a symmetrical binary fluid mixture on a wall

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We study the wetting behavior of a symmetrical binary fluid below the demixing temperature at a nonselective attractive wall. Although it demixes in the bulk, a sufficiently thin liquid film remains mixed. On approaching liquid vapor coexistence, however, the thickness of the liquid film increases and it may demix and then wet the substrate. We show that the wetting properties are determined by an interplay of the two length scales related to the density and the composition fluctuations. The problem is analyzed within the framework of a generic two component Ginzburg-Landau functional (appropriate for systems with short-ranged interactions). This functional is minimized both numerically and analytically within a piecewise parabolic potential approximation. A number of surface transitions are found, including first-order demixing and prewetting, continuous demixing, a tricritical point connecting the two regimes, or a critical end point beyond which the prewetting line separates a strongly and a weakly demixed film. Our results are supported by detailed Monte Carlo simulations of a symmetrical binary Lennard-Jones fluid at an attractive wall.

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I. INTRODUCTION

Phase transitions are well known to be influenced by geometrical confinement [1]. In practice, confinement is often imposed by rigid external constraints, for example, the surfaces of porous or artificially nanostructured media. However, it can also be an inherent feature of a system, as occurs for a liquid wetting film bound to a solid substrate and in equilibrium with its vapor [2]. In such a situation the liquid is confined between the rigid substrate and the flexible liquid-vapor interface.

The effects of confinement are particularly pronounced in the region of critical points. Under such conditions the system exhibits strong order parameter fluctuations, the correlation length of which may become comparable with the linear dimension of the confined system. When this occurs the effects of confinement are felt not just near the confining surfaces, but propagate throughout the system [3].

Critical fluctuation is relevant to the properties of liquid wetting films if the liquid in question possesses an additional internal degree of freedom. Then the state of the liquid is described not only by its number density, but by an additional parameter measuring the degree of internal order. Examples are binary liquids, where the additional order parameter is the relative concentration of species, and ferrofluids where it is the magnetization. In such systems the geometrical constraint (i.e., the film thickness) can itself depend on the state of order in the liquid film. For example, simulation and experiment have recently shown that critical concentration fluctuations can change the equilibrium thickness of a wetting layer of a binary liquid—the so-called critical Casimir effect [4–6].

It transpires, however, that the interesting consequences of interplay between the degree of order in the wetting layer

and film thickness are not limited to the critical point itself. To illustrate this, it is instructive to consider the following *Gedanken* experiment. Let us take a symmetrical binary fluid, i.e., a fluid in which particles of the same species have one strength of interaction, while interactions between dissimilar species have another strength. As elucidated in Ref. [7], it is possible to arrange for such a system to exhibit a second-order line of liquid-liquid demixing transitions terminating at a critical end point (CEP). In general a CEP occurs when a line of second-order phase transitions intersects and is truncated by a first-order phase boundary delimiting a new noncritical phase. In the symmetrical binary fluid mixture, the phase diagram is spanned by three thermodynamic fields (T, μ, h), where T is the temperature, μ is a chemical potential, and h is an ordering field coupling to the relative concentrations of the two fluid components. In this paper we consider the case $h=0$, in which two demixed liquid phases coexist. By tuning T and μ , one finds a critical demixing (or “ λ line”), where the separate liquid phases merge into a single mixed liquid phase. This λ line meets the first-order line of liquid-gas transitions $\mu_\sigma(T)$ at the critical end point (T_e, μ_e) , see Fig. 1(a). For $T < T_e$, the phase boundary $\mu_\sigma(T)$ constitutes a triple line along which the demixed liquid phases coexist with the gas phase, while for $T > T_e$, $\mu_\sigma(T)$ defines the region where the mixed liquid and the gas phase coexist. Precisely at the critical end point the critical liquid mixture coexists with the gas phase. The phase diagram in the density temperature plane is shown in Fig. 1(b).

Suppose now that the fluid is placed in contact with a nonselective attractive substrate (wall) acting equally on both species. If the wall is sufficiently attractive, complete wetting occurs at and above the critical end point temperature T_{CEP} as liquid-vapor coexistence is approached from the vapor

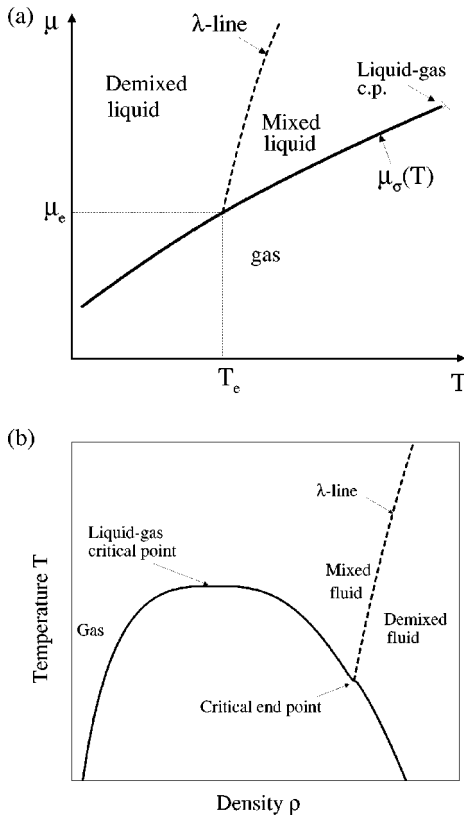


FIG. 1. Schematic phase diagram of the symmetrical binary fluid mixture (a) in the temperature-chemical potential plane and (b) in the density-temperature plane. Dashed line indicates critical demixing transitions, full curve the first-order liquid-vapor coexistence line or envelope, respectively.

side. But what happens for $T < T_{\text{CEP}}$? Far from coexistence, the wetting film is sufficiently thin that demixing will certainly be suppressed. On approaching the coexistence curve, however, the film thickness grows and it is tempting to argue that it eventually exceeds the correlation length of composition fluctuations, whereupon the film spontaneously demixes.

Notwithstanding the appealing simplicity of this argument, it turns out to contain two flaws that render the actual situation rather more complex. First, the thickness of the *mixed* wetting film will not increase beyond all limits below the critical end point T_{CEP} . This is because a hypothetical mixed bulk liquid would not coexist with the vapor phase at the same chemical potential μ_0 as a demixed liquid, but rather at a chemical potential, which is shifted by

$$\mu_* - \mu_0 \propto (T_{\text{CEP}} - T)^{2-\alpha} \quad (1.1)$$

towards the liquid side in the $\mu - T$ plane [8,9]. Since the thickness of the mixed film grows as $\ln(\mu_* - \mu)$ [2,10], it is bounded from above by

$$l_* \propto \ln(\mu_* - \mu_0) \propto \ln(T_{\text{CEP}} - T). \quad (1.2)$$

The maximum thickness l_* of a hypothetical mixed film thus diverges logarithmically on approaching T_{CEP} . In contrast,

the correlation length ξ diverges much faster, like $\xi \propto (T_{\text{CEP}} - T)^{-\nu}$ and will thus always exceed l_* sufficiently close to T_{CEP} .

The second flaw in our argument is its implicit assumption that the composition or order parameter profile is confined in an effectively steplike density profile, i.e., that the interfacial width between the liquid and the vapor is much smaller than the correlation length of composition fluctuations. Although this is true in the region of the critical end point, for temperature sufficiently below T_{CEP} the correlation lengths of density and composition fluctuations can be comparable and the interplay between the two subtle.

In the present paper, we deploy a mean-field calculation and Monte Carlo simulation to elucidate the range of possible wetting behavior of a symmetrical binary fluid mixture at a nonselective attractive wall for temperatures below T_{CEP} . For the sake of simplicity, we have chosen to ignore long-range dispersion forces in the analytical calculations, instead taking the interactions to be short ranged. This allows us to base our study on a generic Ginzburg-Landau model, which we solve numerically and analytically within a square gradient approximation. The latter leads to the construction of a film free energy (effective interface potential) highlighting the role of the different length scales involved in the problem. We show that the competition of length scales results in wetting phase behavior considerably more complex than has hitherto been appreciated. The analytical results are compared with (and supported by) detailed Monte Carlo simulations of a binary Lennard-Jones fluid in a semi-infinite geometry, interacting with a nonselective attractive substrate via dispersion forces.

With regard to previous related work, the sole discussion of wetting of symmetrical binary fluids at a nonselective wall (of which we are aware) is that of Dietrich and Schick [11] who considered them in a sharp kink approximation treatment of binary fluids having long-ranged interactions. Most other work on the wetting properties of binary fluids has focused on the case of a selective substrate (favoring one component) [10–14]. Although such models correspond more closely than ours to experimental conditions [10,15], they lack the aspect of simultaneous demixing ordering and wetting, which is of interest to us here. It should be stressed, however, that realizations of fluids having symmetrical internal degrees of freedom do in fact exist, notably in the form of ferrofluids [16], so our model is of more than purely theoretical interest.

More general studies of wetting in systems with more than one order parameter and associated length scales have been discussed by Hauge [17], who pointed out that wetting exponents may become nonuniversal even on the mean-field level due to the competition of length scales. Later studies have often focused on this nonuniversality, e.g., in the context of wetting phenomena in superconductors [18], alloys [19,20], and related systems [21].

The present paper is organized as follows. In Sec. II we introduce our Ginzburg-Landau free-energy functional and obtain its wetting behavior in the limits of infinite and vanishing order-parameter stiffness. At intermediate values of the stiffness parameter the wetting behavior is found firstly

via an analytical minimization of the functional within a piecewise parabolic potential approximation (Sec. II B), and then (in Sec. II C) via a numerical minimization of the free-energy functional to obtain the density order parameter profiles. In Sec. III A we report the results of grand canonical Monte Carlo studies of a symmetrical binary Lennard-Jones fluid at an attractive structureless wall. The density and order-parameter profiles with respect to the wall are obtained along a subcritical isotherm for a number of different wall-fluid potential strengths. Finally we compare and discuss the mean-field and simulation results in Sec. IV.

II. GINZBURG-LANDAU THEORY

Our theoretical studies are based on a generic Ginzburg-Landau functional for a system with two order parameters $\phi(\vec{r}, z)$ and $m(\vec{r}, z)$:

$$\mathcal{F} = \int d\vec{r} \int_0^\infty dz \left\{ \frac{g}{2} (\nabla \phi)^2 + \frac{\gamma}{2} (\nabla m)^2 + f(m, \phi) \right\} + \int d\vec{r} f_s(m, \phi)|_{z=0} \quad (2.1)$$

with the bulk free-energy density

$$f(m, \phi) = -\frac{a_\phi}{2} \phi^2 + \frac{b_\phi}{4} \phi^4 - \frac{a_m}{2} m^2 + \frac{b_m}{4} m^4 + \mu \phi - \kappa m^2 \phi \quad (2.2)$$

and the bare surface free energy at the wall

$$f_s(m, \phi) = \frac{C_\phi}{2} \phi^2 + H_\phi \phi + \frac{C_m}{2} m^2. \quad (2.3)$$

The z axis is taken to be perpendicular to the wall and $\int d\vec{r}$ integrates over the remaining spatial dimensions. In our case, the quantity m is related to the difference between the partial densities of the two components, $m \propto (\rho_A - \rho_B)$, and ϕ to the total density, $\phi \propto (\rho - \rho_0)$, where the reference density ρ_0 is chosen in the liquid-vapor coexistence region such the cubic term proportional to $(\rho - \rho_0)^3$ in Eq. (2.2) vanishes. Below the liquid-vapor critical point, it is convenient to set the units of ϕ , m , F and of the length such that $b_m = b_\phi = a_\phi = g = 1$, and to define $\theta = a_m - 1$. The bulk free-energy density then takes the form

$$f(m, \phi) = -\frac{1}{2} \phi^2 + \frac{1}{4} \phi^4 - \frac{\theta}{2} m^2 + \frac{1}{4} m^4 - \mu \phi + \kappa (1 - \phi) m^2. \quad (2.4)$$

The bulk properties of this model have been discussed earlier [7]. A λ -line $\theta_\lambda(\mu)$ of continuous transitions separates the mixed fluid from the demixed fluid at large negative μ , corresponding to large densities ϕ . As long as $\kappa < 1$, it is terminated by the onset of liquid-vapor coexistence at a critical end point ($\theta_{\text{CEP}} = 0$, $\mu_{\text{CEP}} = 0$). The parameter μ is field like and θ is temperaturelike, $\theta \propto (T - T_{\text{CEP}})$, where T_{CEP} is the

critical end-point temperature. Above θ_{CEP} , liquid-vapor coexistence is encountered at $\mu = 0$, and below θ_{CEP} , at

$$\mu_c = \frac{\theta^2}{8(1 - \kappa^2)}. \quad (2.5)$$

The coexisting liquid and gas phases are characterized by the order parameters (to linear order in μ)

$$m_-^* = 0, \quad \phi_-^* = -1 - \mu/2 \quad (2.6)$$

in the gas phase, and

$$m_+^* = \frac{\theta - \kappa \mu}{1 - \kappa^2}, \quad \phi_+^* = 1 - \frac{\mu}{2} + \frac{\kappa}{2} m_+^{*2} \quad (2.7)$$

in the liquid phase. These expressions are also valid in the regime where the liquid or gas phase are metastable.

Minimizing the functional (2.1) yields the Euler Lagrange equations

$$g \frac{d^2 \phi}{(dz)^2} = \frac{\partial f}{\partial \phi}, \quad \gamma \frac{d^2 m}{(dz)^2} = \frac{\partial f}{\partial m}, \quad (2.8)$$

with the boundary conditions

$$g \left. \frac{d\phi}{dz} \right|_{z=0} = \frac{\partial f_s}{\partial \phi}, \quad \gamma \left. \frac{dm}{dz} \right|_{z=0} = \frac{\partial f_s}{\partial m}. \quad (2.9)$$

We wish to study a situation where the mixed liquid ($m \equiv 0$) wets the wall at $\mu = 0$ (coexistence between vapor and mixed liquid). To ensure this under all circumstances, we choose $H_\phi = -\phi_0 C_\phi$ with $\phi_0 > \phi_+^*$ and take the limit $C_\phi \rightarrow \infty$, which is equivalent to constraining the surface density at the fixed value $\phi(0) = \phi_0$. The surface coupling C_m is taken to be positive. It accounts for weakening of the demixing tendency at the surface due to the reduced number of interacting neighbors.

One possible solution of the Euler-Lagrange equations describes a mixed film at a wall. In this case, $m(z) = 0$ everywhere and one is left with one order parameter ϕ only. The bulk value of ϕ in the metastable mixed phase is $\phi_+^{(0)} = 1 - \mu/2$. The standard way of solving the problem [2] shall be sketched briefly for future reference. One begins by identifying the integration constant

$$\frac{1}{2} \left(\frac{d\phi}{dz} \right)^2 - f(\phi) + f(\phi_-^{(0)}) \equiv 0, \quad (2.10)$$

which gives an expression for $d\phi/dz$ as a function of ϕ . The surface free energy can then be expressed as an integral over ϕ

$$F_{\text{exc}}^{(0)} = \int_{\phi_-^{(0)}}^{\phi_0} d\phi \sqrt{2[f(\phi) - f(\phi_-^{(0)})]} \quad (2.11)$$

and the excess density $\phi_{\text{exc}}^{(0)} = 1/2 \int_0^\infty dz [\phi(z) - \phi_-^{(0)}]$ at the surface can be calculated *via*

$$\phi_{\text{exc}}^{(0)} = \frac{1}{2} \int_{\phi_-^{(0)}}^{\phi_0} \frac{d\phi(\phi - \phi_-^{(0)})}{\sqrt{2[f(\phi) - f(\phi_-^{(0)})]}}. \quad (2.12)$$

As long as $|f(\phi_+^{(0)} - f(\phi_-)| \ll (\phi_+^{(0)} - \phi_-)^2 f''(\phi_+^{(0)})$, which is true for $\mu \ll 2$, the main contribution to this integral stems from ϕ values around $\phi_+^{(0)}$. The numerator in the integrand can then be expanded around $\phi_+^{(0)}$. Carrying this to second order and assuming $\mu \ll (\phi_0 - \phi_+^{(0)})$, one obtains

$$\phi_{\text{exc}}^{(0)} \approx \sqrt{\frac{1}{2}} \ln \left(\frac{2}{\phi_+^{(0)} - \phi_0} \right), \quad (\phi_0 < \phi_+^{(0)}), \quad (2.13)$$

$$\phi_{\text{exc}}^{(0)} \approx \sqrt{\frac{1}{2}} \ln \left(\frac{4(\phi_0 - \phi_+^{(0)})}{\mu} \right), \quad (\phi_0 > \phi_+^{(0)}). \quad (2.14)$$

Above the bulk demixing transition, the mixed film thus wets the wall at coexistence ($\mu \rightarrow 0$) for $\phi_0 > \phi_+^{(0)}$, and maintains a finite thickness for $\phi_0 < \phi_+^{(0)}$. We will choose $\phi_0 > \phi_+^{(0)}$ hereafter. From Eq. (2.11), one calculates the surface free energy to leading order in μ and $(\phi_0 - \phi_+^{(0)})$

$$F_{\text{exc}}^{(0)} = \frac{2\sqrt{2}}{3} + \frac{1}{\sqrt{2}} (\phi_0 - \phi_+^{(0)})^2. \quad (2.15)$$

Below the bulk demixing transition, $\mu = \mu_c > 0$ at coexistence and the thickness of the mixed film remains finite under all circumstances.

In the following, we shall first analyze the wetting behavior for the limiting cases where the order parameter varies on very short length scales ($\gamma/m_+^{*2} \rightarrow 0$) and on long length scales ($\gamma/m_+^{*2} \rightarrow \infty$) compared to the density. Then we will discuss the general case of intermediate γ , first analytically in an approximation where the potential (2.4) is replaced by a piecewise quadratic potential, and then numerically with the full potential (2.4).

A. Limiting cases

We consider first the wetting behavior at ($\gamma/m_+^{*2} \rightarrow 0$). In this case, m adapts locally to ϕ , and the order parameter profile $m(z)$ can be written as $m[\phi(z)]$ with $m(\phi) = \theta + 2\kappa(\phi - 1)$ for $\phi < 1 - \theta/2\kappa$ and $m(\phi) = 0$ otherwise. Hence we are left with the effective one order parameter problem of calculating the density profile $\phi(z)$ in the slightly altered potential $\hat{f}(\phi) = f[m(\phi), \phi]$. Since $\hat{f}(\phi)$ is a smooth function with two minima, one can proceed as sketched above for the mixed film, with the analogous result: The demixed film wets the wall at $\phi > \phi_+^*$.

The analysis of the opposite case, ($\gamma/m_+^{*2} \rightarrow \infty$), is somewhat more involved. Here ϕ adapts locally to m ; however, the bulk equation $\partial f / \partial \phi = \phi^3 - \phi + \mu - \kappa m^2 = 0$ has two solutions $\phi_{\pm}(m)$. One conveniently separates the profiles into four parts (I)–(IV) as indicated in Fig. 2. The regions (I) and (III) are narrow slabs where $\phi(z)$ varies rapidly and m can be approximated by a constant, $m = m_0$ at the surface (I) and m_2 at the interface (III). In region (I), ϕ drops from its surface value ϕ_0 to the local equilibrium value $\phi_+(m_0)$, and

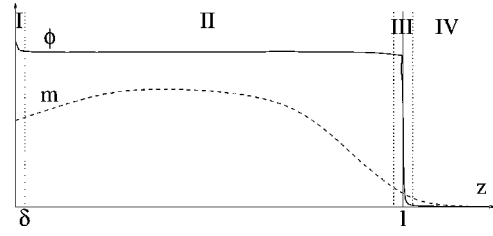


FIG. 2. Schematic sketch of density and order parameter profiles in the limit $\gamma/m_+^{*2} \rightarrow \infty$. See text for more explanation.

in region (III), it switches from $\phi_+(m_2)$ to $\phi_-(m_2)$. The other two regions, (II) and (IV), are much wider; the order parameter $m(z)$ varies slowly and $\phi(z)$ adjusts locally to $m(z)$, such that $\phi = \phi_+(m)$ in region (II) and $\phi = \phi_-(m)$ in region (IV).

To make the argument more quantitative, we specify the actual subdivision of the excess free energy of Eq. (2.1),

$$\mathcal{F}_{\text{exc}} = f_s(m_0, \phi_0) + \mathcal{F}_I + \mathcal{F}_{II} + \mathcal{F}_{III} + \mathcal{F}_{IV} \quad (2.16)$$

with

$$\mathcal{F}_I = \int_0^\delta dz \left[\frac{1}{2} \left(\frac{d\phi}{dz} \right)^2 + f(m_0, \phi) - f[m_0, \phi_+(m_0)] \right]$$

$$\mathcal{F}_{II} = \int_0^l dz \left[\frac{1}{2} \gamma \left(\frac{dm}{dz} \right)^2 + f[m, \phi_+(m)] \right],$$

$$\begin{aligned} \mathcal{F}_{III} = & \int_{l-\delta}^l dz \left[\frac{1}{2} \left(\frac{d\phi}{dz} \right)^2 + f(m_2, \phi) - f[m_2, \phi_+(m_2)] \right] \\ & + \int_l^{l+\delta} dz \left[\frac{1}{2} \left(\frac{d\phi}{dz} \right)^2 + f(m_2, \phi) - f[m_2, \phi_-(m_2)] \right], \end{aligned}$$

$$\mathcal{F}_{IV} = \int_0^l dz \left[\frac{1}{2} \gamma \left(\frac{dm}{dz} \right)^2 + f[m, \phi_-(m)] \right].$$

The calculation for the regions (I), (III), and (IV) can proceed in an analogous way as sketched earlier for the mixed film: The profiles of $\phi(z)$ in regions (I), (III), and of $m(z)$ in region (IV) are monotonic and the integration constant [cf. Eq. (2.10)] is known (zero). One obtains to leading order in μ and $[\phi_0 - \phi_+(m_0)]$

$$F_I = \sqrt{\frac{1}{2}} [\phi_0 - \phi_+(m_0)]^2 + \dots, \quad (2.17)$$

$$F_{III} = \frac{2\sqrt{2}}{3} + \mathcal{O}[(u - \kappa m_2^2)^2], \quad (2.18)$$

$$F_{IV} = \frac{m_2^2}{2} \sqrt{\gamma(4\kappa + \kappa\mu - \theta)}. \quad (2.19)$$

In the region (II), the integration constant is unknown,

$$\frac{1}{2} \gamma \left(\frac{dm}{dz} \right)^2 - f[m, \phi_+(m)] = p, \quad (2.20)$$

with $p > 0$ if the profile of $m(z)$ is monotonic, and $p < 0$ if $m(z)$ is nonmonotonic, like in Fig. 2. A connection between p and the width l of the film can be established using $l = \int_{m_2}^{m_0} dm / |dm/dz|$ in the first case, and

$$l = \int_{m_0}^{m_{\max}} \frac{dm}{|dm/dz|} + \int_{m_2}^{m_{\max}} \frac{dm}{|dm/dz|}$$

in the second case, where m_{\max} solves $p = -f[m_{\max}, \phi_+(m_{\max})]$. Next we expand the function $f[m, \phi_+(m)]$ about its minimum m_+^* , leading to

$$f[m, \phi_+(m)] \approx (1 - \kappa^2) m_+^4 \left[\left(\frac{m}{m_+^*} - 1 \right)^2 - \frac{1}{4} \right]. \quad (2.21)$$

One deduces the characteristic length scale,

$$\lambda = \sqrt{\frac{\gamma}{2(1 - \kappa^2)}} \frac{1}{m_+^*}, \quad (2.22)$$

which grows very large in the limit $\gamma/m_+^{*2} \rightarrow \infty$. The result for \mathcal{F}_I can therefore be expanded in powers of $e^{-l/\lambda}$. After adding up all contributions regions (I)–(IV) and minimizing with respect to m_2 , the total excess free energy of the demixed film takes the form $F_{\text{exc}} = F_{\text{surf}}(m_0, \phi_0) + F_{\text{int}} + V(l)$ with the surface contribution

$$F_{\text{surf}} = f_s(m_0, \phi_0) + \sqrt{\frac{1}{2}} [\phi_0 - \phi_+(m_0)]^2 + 8\lambda \mu_c (1 - m_0/m_+^*)^2, \quad (2.23)$$

the interface contribution

$$F_{\text{int}} = \frac{2\sqrt{2}}{3} + 8\lambda \mu_c, \quad (2.24)$$

and a surface interface interaction term

$$V(l) = 2(\mu - \mu_c)l - 32\lambda \mu_c (1 - m_0/m_+^*) e^{-l/\lambda} + 16\lambda \mu_c [A - (1 - m_0/m_+^*)^2 B] e^{-2l/\lambda}, \quad (2.25)$$

where $B = [\lambda \sqrt{\gamma[\kappa - m_+^{*2}(1 - \kappa^2)]/4}]^{-1}$, and $A = -3$ or $A = 1$, depending on whether or not the profile $m(z)$ is monotonic.

The result can now be discussed. At $m_0 < m_+^*$, the leading term $e^{-l/\lambda}$ of the potential $V(l)$ is attractive, and wetting is not possible. At $m_0 > m_+^*$, an infinitely thick demixed film is metastable at coexistence. Its free-energy difference to the mixed film $\Delta F = F_{\text{exc}} - F_{\text{exc}}^{(0)}$ is up to third order in m_+^*

$$\Delta F = \frac{1}{\sqrt{2}} [\sqrt{\gamma(1 - \kappa^2)} [1 + (1 - m_0/m_+^*)^2] m_+^{*3} + \{C_m/\sqrt{2} - \kappa[\phi_0 - \phi_+(m_0)]\} m_0^2]. \quad (2.26)$$

The limit $\gamma/m_+^{*2} \rightarrow \infty$ can be taken in two ways: either $\gamma \rightarrow \infty$ at fixed m_+^* , or $m_+^* \rightarrow 0$ at fixed γ . In the first case the

first term in Eq. (2.26) dominates and the free energy of the demixed film exceeds that of the mixed film: The film remains mixed and dewets accordingly.

The second case is more subtle. Here, the second term dominates, and the free energy of the mixed film may be less favorable, depending on the ratio of C_m and $(\phi_0 - \phi_+^*)$. Note that the density enhancement at the surface, $\sqrt{2}\kappa(\phi_0 - \phi_+^*)$, acts as an additional surface coupling, which opposes the effect of C_m . The parameter C_m accounts for the direct reduction of interacting neighbors right at the surface. It is counterbalanced by the fact that the density ϕ_0 close to the surface is higher than in the bulk. If the latter effect dominates, the film demixes at the surface even for $m_+^* \rightarrow 0$ or $T \rightarrow T_{\text{cep}}$.

B. Analytical results in a piecewise parabolic potential

At fixed m_+^* , we have seen that the demixed film wets the substrate in the limit $\gamma \rightarrow 0$, where the order parameter m varies much faster than the density ϕ , and dewets at $\gamma \rightarrow \infty$, where the density varies much faster than the order parameter. Now we consider intermediate values of γ , where the two characteristic length scales become comparable. Far from the critical end point, this is the usual case in a binary liquid, since the interaction ranges responsible for liquid-gas separation and demixing are comparable.

In order to carry further the analytical analysis, we approximate the free-energy density $f(\phi, m)$ (2.4) by a piecewise quadratic form

$$f(\phi, m) = \frac{1}{2} (\phi - \tilde{\phi}, m - \tilde{m}) \tilde{f} \begin{pmatrix} \phi - \tilde{\phi} \\ m - \tilde{m} \end{pmatrix} + \sigma \tilde{\mu}, \quad (2.27)$$

with three pieces corresponding to the gas phase and the two liquid phases, separated by the lines

$$\phi_{\text{sep}}(m) = -\kappa(m^2 + m_+^{*2} - |m|_+^*) + \tilde{\mu}/2 \quad (2.28)$$

and $m \equiv 0$ at $\phi > \phi_{\text{sep}}(0)$. Here $\tilde{\mu} = \mu - \mu_c$, $\sigma = -1$ for $\phi > \phi_{\text{sep}}(m)$ (gas phase), $\sigma = +1$ for $\phi < \phi_{\text{sep}}(m)$ (liquid phases), and the parabolae are adjusted to the leading terms in the expansion of the functional (2.4) about its minima,

$$\begin{pmatrix} \tilde{\phi} \\ \tilde{m} \end{pmatrix} = \begin{pmatrix} -1 \\ 0 \end{pmatrix}, \quad \tilde{f} = \begin{pmatrix} 2 & 0 \\ 0 & 4\kappa \end{pmatrix}, \quad (2.29)$$

for $\phi < \phi_{\text{sep}}(m)$ (gas phase), and

$$\begin{pmatrix} \tilde{\phi} \\ \tilde{m} \end{pmatrix} = \begin{pmatrix} 1 + \kappa m_+^{*2}/2 \\ \pm m_+^* \end{pmatrix}, \quad \tilde{f} = \begin{pmatrix} 2 & \mp 2\kappa m_+^* \\ \mp 2\kappa m_+^* & 2m_+^{*2} \end{pmatrix}, \quad (2.30)$$

for $\phi > \phi_{\text{sep}}(m)$ (liquid phases), where the upper sign holds for $m > 0$, the lower for $m < 0$. The choice (2.28) of ϕ_{sep} ensures that the potential $f(m, \phi)$ is continuous.

In such a potential, profiles of demixed films correspond to paths in the (ϕ, m) space, which can be separated into three parts: (i) moving in one of the liquid regions from (ϕ_0, m_0) to $(\phi_1, m = 0)$; (ii) following the edge ($m \equiv 0$) be-

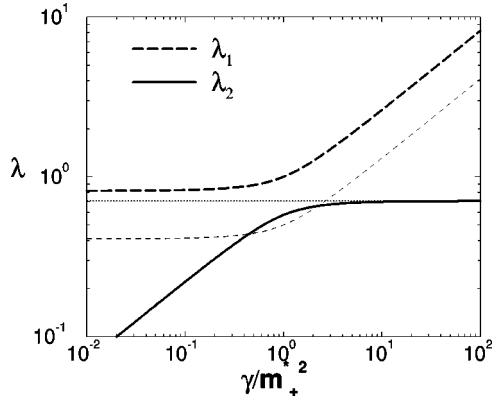


FIG. 3. Length scales λ_1 and λ_2 vs γ/m_+^{*2} at $\kappa=0.5$. Thin line shows $\lambda_1/2$ for comparison.

tween the two liquid regions from $(\phi_1, 0)$ to $[\phi_{\text{sep}}(0), 0]$; (iii) moving in the gas region from $[\phi_{\text{sep}}(0), 0]$ to $(-1, 0)$. On principle, a direct transition from (i) to (iii) is conceivable. For the parameters ϕ_0 of interest, however, such profiles turn out to be energetically less favorable than the profiles that have an intermediate (ii). Profiles of mixed films have two parts (ii) and (iii) only. We shall denote $l_{(i)} \equiv l$, $l_{(ii)}$, and $l_{(iii)}$, the length of the slab spent in regions (i), (ii), or (iii), respectively.

At given slab length and boundary conditions, the free energy in each of the slabs can be calculated exactly using

$$\int_0^l dz \frac{1}{2} \left\{ \left(\frac{du}{dz} \right)^2 + \frac{u^2}{\lambda^2} \right\} = \frac{1}{4} \left\{ [u(0) + u(l)]^2 \tanh \frac{l}{2\lambda} + [u(0) - u(l)]^2 \coth \frac{l}{2\lambda} \right\}. \quad (2.31)$$

The calculation is straightforward in the regimes (ii) and (iii). In regime (i), the free-energy functional has to be diagonalized first:

$$\mathcal{F}_{(i)} = \frac{1}{2} \int_0^l dz \left\{ \left[\left(\frac{dv}{dz} \right)^2 + \frac{v^2}{\lambda_1^2} \right] + \left[\left(\frac{dw}{dz} \right)^2 + \frac{w^2}{\lambda_2^2} \right] \right\}$$

with

$$\lambda_{1,2}^{-2} = 1 + \frac{m_+^{*2}}{\gamma} \mp \sqrt{\left(\frac{m_+^{*2}}{\gamma} \right)^2 + \frac{m_+^{*2}}{\gamma} (4\kappa^2 - 2) + 1}, \quad (2.32)$$

$$\begin{pmatrix} v \\ w \end{pmatrix} = \frac{1}{\sqrt{e^\delta + e^{-\delta}}} \begin{pmatrix} e^{-\delta/2} & e^{\delta/2} \\ e^{\delta/2} & -e^{-\delta/2} \end{pmatrix} \begin{pmatrix} \phi - \bar{\phi} \\ \sqrt{\gamma(m - \bar{m})} \end{pmatrix},$$

where we have defined

$$\delta = \frac{1}{2} \ln \left(\frac{2 - \lambda_1^{-2}}{\lambda_2^{-2} - 1} \right). \quad (2.33)$$

The parameter δ or alternatively γ/m_+^{*2} determines the wetting behavior. Figure 3 shows the two length scales λ_1 and

λ_2 as a function of γ/m_+^{*2} . The length λ_1 is always larger than λ_2 . At $\gamma/m_+^{*2} \gg 1$ or $\delta \gg 0$, it characterizes the spatial variations of $m(z)$ and grows linearly with γ/m_+^{*2} ; at $\gamma/m_+^{*2} \ll 1$ or $\delta \ll 0$, it characterizes the variations of $\phi(z)$ and remains largely independent of γ/m_+^{*2} . These are the limiting regimes discussed in the previous subsection. At $\gamma/m_+^{*2} \approx 1$ or $\delta \approx 0$, both λ_1 and λ_2 are related to linear combinations of $\phi(z)$ and $m(z)$ [22].

The further calculation proceeds as follows: The free energy in regime (iii) is given by

$$F_{(i)} = \sqrt{2}/2 \{ 1 + [\phi_{\text{sep}}(0) + 1]^2 \}. \quad (2.34)$$

In the region (ii), the result for the free energy is expanded in powers of $e^{-\sqrt{2}l_{(ii)}}$ up to the second order and minimized with respect to $l_{(ii)}$. The free energy calculated in region (i) is expanded up to second order in powers of e^{-l/λ_1} and up to first order in e^{-l/λ_2} , where $l \equiv l_{(i)}$. The three contributions are then added up, and the sum is minimized with respect to ϕ_1 and m_0 at given surface coupling C_m . The solution has to be compared with the free energy of a mixed film, which is calculated analogously.

We only report the result for the case $C_m = 0$ here. The expressions obtained for arbitrary C_m are more complicated, but qualitatively similar. Without loss of generality, we can assume $m > 0$ in the demixed film. As long as $m_0 > 0$, the surface order parameter m_0 and the free-energy difference ΔF , between the mixed and demixed film, can then be expanded as

$$\begin{aligned} \sqrt{\gamma} m_0 &= \sqrt{\gamma} m_+^* + \iota_0 + \iota_1 e^{-l/\lambda_1} + \iota_2 e^{-l/\lambda_2} + \iota_3 e^{-2l/\lambda_1}, \\ \Delta F(l) &= \Delta F_{(ii)} + \tau_0 + \tau_2 e^{-l/\lambda_1} + \tau_2 e^{-l/\lambda_2} + \tau_3 e^{-2l/\lambda_1}. \end{aligned} \quad (2.35)$$

Using the abbreviations

$$K_0 = \frac{e^\delta + e^{-\delta}}{\lambda_1 \lambda_2} \quad \text{and} \quad K_\pm = \frac{\lambda_1 \lambda_2}{e^{\pm \delta} \lambda_1 + e^{\mp \delta} \lambda_2},$$

the coefficients can be written as

$$\begin{aligned} \iota_0 &= (\lambda_2^{-1} - \lambda_1^{-1}) K_- (\phi_0 - \bar{\phi}), \\ \iota_{1,2} &= -2K_0 K_+ K_- e^{\pm \delta} \sqrt{\gamma} m_+^* \\ \iota_3 &= -2K_0 K_-^2 (1 + 8K_+ e^{-\delta/\lambda_1}) (\phi_0 - \bar{\phi}), \end{aligned} \quad (2.36)$$

$$\tau_0 = K_0 [K_+ \gamma m_+^{*2} + K_- (\phi_0 - \bar{\phi})^2],$$

$$\tau_{1,2} = \pm 2K_0 K_+ K_- / \lambda_{2,1} \sqrt{\gamma} m_+^* (\phi_0 - \bar{\phi}),$$

$$\begin{aligned} \tau_3 &= K_0 K_- K_+^2 e^\delta (e^{-\delta/\lambda_2} - e^{\delta/\lambda_1}) / \lambda_2 \gamma m_+^{*2} \\ &\quad + K_0 K_-^2 e^{-\delta} (1 + 8K_+ e^{-\delta/\lambda_1}) / \lambda_2 (\phi_0 - \bar{\phi})^2, \end{aligned} \quad (2.37)$$

and with $h = m_+^{*4} (1 - \kappa^2) - 2\bar{\mu}$, $p = \phi_0 - \bar{\phi} + \kappa m_+^{*2}$,

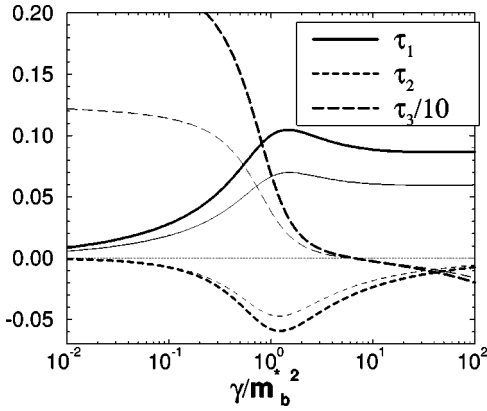


FIG. 4. Coefficients τ_i of interfacial potential vs γ/m_+^{*2} for $\kappa=0.5$, $\Phi_0=1.5$, and surface coupling $C_m=0$ (thick lines) and $C_m=0.2$ (thin lines).

$$\Delta F_{(ii)} = -\frac{1}{\sqrt{2}}p^2 - \frac{h}{2\sqrt{2}} \left(1 + \ln \frac{dp^2}{h} \right). \quad (2.38)$$

When taking the limits $\delta \rightarrow \pm\infty$, one recovers qualitatively [23] the behavior discussed in the previous section.

The function $\Delta F(l)$ can be conceived as an effective interface potential for the demixed film. The parameters τ_i for a choice of ϕ_0 ($\phi_0=1.5$) and two values of C_m , $C_m=0$ according to Eq. (2.37) and $C_m=0.02$, are shown in Fig. 4. One finds that τ_1 is always positive, τ_2 is always negative, and τ_3 changes sign from positive to negative as γ/m_+^{*2} increases. The leading term of the potential $F(l)$ is thus positive, and one expects a first-order wetting transition and a prewetting line. On the other hand, the expansions (2.35) are only valid as long as the surface order parameter m_0 is positive. According to Eq. (2.36), the coefficients ν_i of the expansion for $m_0(l)$ are negative except for the zeroth-order term ν_0 . Hence m_0 decreases with film thickness and may vanish at some thickness l_c . In this case, the film mixes continuously at l_c , and the prewetting line turns into a second-order demixing line sufficiently far from coexistence.

C. Numerical solution

The analytical results of the Sec. II B provided insight into the competition of length scales in the binary fluid and the wetting scenarios, which can be expected on a wall as a result. However, a reliable calculation of actual phase diagrams, including the details of the prewetting line, is not possible on the basis of the expansion (2.35). We have thus supplemented the analytical work by a numerical minimization of the functional (2.1) in the $\mu - \phi_0$ plane for selected sets of parameters γ and C_m .

The problem is simplified considerably due to the fact that $\phi(z)$ is a monotonic function of z , i.e., $m(z)$ can be expressed as a function $m(\phi)$. The bulk free-energy functional in Eq. (2.1) can thus be rewritten as

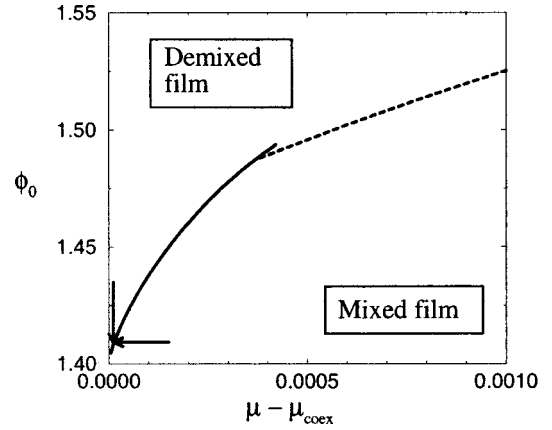


FIG. 5. Phase diagram in the $\mu - \phi_0$ plane. Parameters are $\kappa=0.5$, $\theta=0.1$, and $\gamma=1.$, $C_m=0.2$. Solid line indicates first-order transition, dashed line second-order transition.

$$\begin{aligned} \mathcal{F} &= \int_0^\infty dz \left\{ \frac{1}{2} \left[1 + \gamma \left(\frac{dm}{d\phi} \right)^2 \right] \left(\frac{d\phi}{dz} \right)^2 + f[m(\phi), \phi] \right\} \\ &= \int_{\phi_-^*}^{\phi_0} d\phi \sqrt{1 + \gamma \left(\frac{dm}{d\phi} \right)^2} \sqrt{f[m(\phi), \phi] - f(0, \phi_-^*)}, \end{aligned}$$

where the integration constant (2.10) has been identified and exploited as usual. Minimization with respect to the function $m(\phi)$ leads to the Euler-Lagrange equation

$$2\gamma f(m, \phi) \frac{d^2 m}{d\phi^2} = \left[1 + \gamma \left(\frac{dm}{d\phi} \right)^2 \right] \left(\frac{\partial f}{\partial m} - \gamma \frac{dm}{d\phi} \frac{\partial f}{\partial \phi} \right), \quad (2.39)$$

which we have solved using the Verlet algorithm.

Some results are shown in Figs. 5, 6, 7, and 8. As anticipated in the Sec. II B, we find a first-order wetting transition, a discontinuous prewetting line, and a continuous demixing line. At surface coupling $C_m > 0$, the demixing line joins the prewetting line in a surface critical end point (Fig. 5). The prewetting line separates a demixed thick film from a mixed thin film (see profiles in Fig. 6) before reaching the critical end point, then two demixed films of different thickness, and

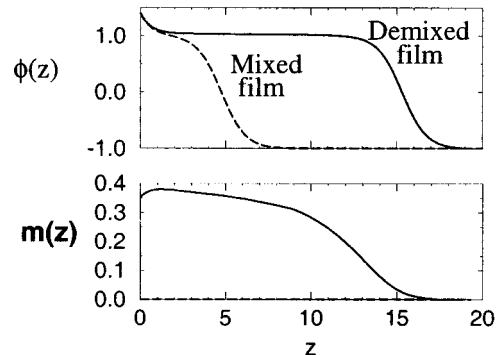


FIG. 6. Density and order-parameter profiles for the coexisting mixed and demixed film at the point in the $\mu - \phi_0$ plane indicated by the arrows in Fig. 6.

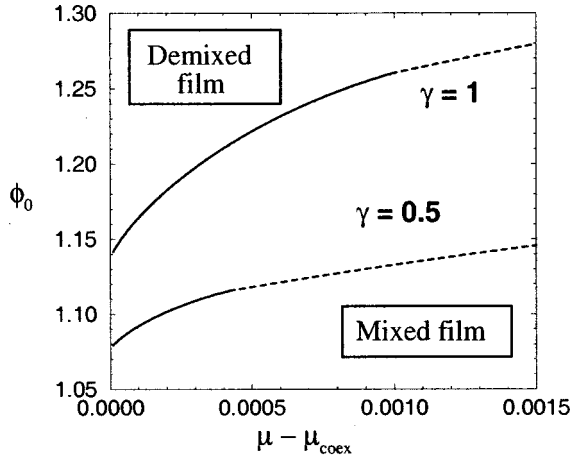


FIG. 7. Phase diagrams in the $\mu - \phi_0$ plane for different γ with $\theta=0.1$, surface coupling $C_m=0$, and parameters as in Fig. 6 otherwise. Solid lines indicate first-order transition, dashed lines second-order transitions.

finally vanishes in a critical point. On decreasing the surface coupling C_m , the critical end point and the critical point move closer to each other, until they merge in a surface tricritical point.

Figure 7 shows two cases of phase diagrams in the $\phi_0 - \mu$ plane for $C_m=0$ and two different γ at fixed θ , i.e., at fixed bulk order parameter m_+^* . With increasing γ , the prewetting line shifts towards larger ϕ_0 and extends deeper into the off-coexistence region. As $\gamma \rightarrow \infty$, it moves to $\phi_0 \rightarrow \infty$, the film remains mixed and thin at all finite ϕ_0 . At $\gamma \rightarrow 0$, on the other hand, the line becomes flat, approaches ϕ_+^* , and the tricritical point where it turns into a second-order line moves to $\mu_t \rightarrow \mu_c$. The numerical results thus agree with the conclusions from Sec. II A.

Figure 8 demonstrates what happens if instead of making γ larger, one increases the characteristic length scale of order parameter fluctuations by decreasing θ , i.e., approaching the critical end point (reducing m_+^*). Far from liquid-vapor coexistence, the transition line still moves towards larger ϕ_0 . However, the effect reverses close to coexistence, the demix-

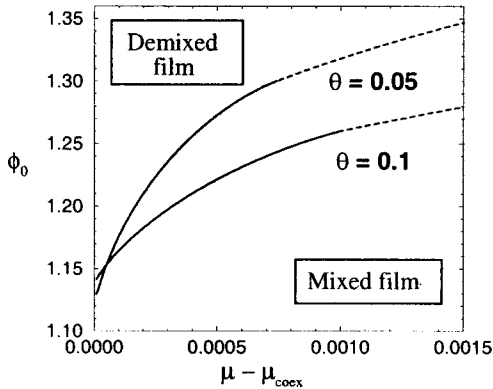


FIG. 8. Phase diagrams in the $\mu - \phi_0$ plane for different θ with $\gamma=1$, surface coupling $C_m=0$, and parameters as in Fig. 6 otherwise. Solid lines indicate first-order transition, dashed lines second-order transitions.

ing transition is now shifted to lower surface densities ϕ_0 . Furthermore, the length of the prewetting line shrinks instead of growing.

III. MONTE CARLO SIMULATIONS

In this section we describe Monte Carlo simulation studies of the subcritical wetting behavior of a symmetrical binary fluid at a structureless wall.

A. Model and simulation details

The system we have studied is a symmetrical binary fluid, having interparticle interactions of the Lennard-Jones (LJ) form:

$$u(r_{ij}) = 4\epsilon_{ij} \left[\left(\frac{\sigma_{ij}}{r_{ij}} \right)^{12} - \left(\frac{\sigma_{ij}}{r_{ij}} \right)^6 \right]. \quad (3.1)$$

We made the following choice of model parameters: $\sigma_{11} = \sigma_{22} = \sigma_{12} = \sigma = 1$; $\epsilon_{11} = \epsilon_{22} = \epsilon$; and $\epsilon_{12} = 0.7\epsilon$, i.e., interactions between similar species are treated identically, but those between unlike species are weakened. The interparticle potential was truncated at a distance of $R_c = 2.5\sigma$ and no long-range correction or potential shift was applied.

The fluid was confined within a cuboidal simulation cell having dimensions $P_x \times P_y \times D$, in the x , y , and z coordinate directions, respectively, with $P_x = P_y = P$. The simulation cell was divided into cubic subcells (of size the cutoff R_c) in order to aid identification of particle interactions. Thus $P = pR_c$ and $D = dR_c$, with p and d both integers. To approximate a semi-infinite geometry, periodic boundary conditions were applied in the x and y directions, while hard walls were applied in the unique z direction at $z=0$ and $z=D$. The hard wall at $z=0$ was made attractive, using a potential designed to mimic the long-ranged dispersion forces between the wall and the fluid [24]:

$$V(z) = \epsilon_w \left[\frac{2}{15} \left(\frac{\sigma_w}{z} \right)^9 - \left(\frac{\sigma_w}{z} \right)^3 \right]. \quad (3.2)$$

Here z measures the perpendicular distance from the wall, ϵ_w is a ‘‘well depth’’ controlling the interaction strength, and we set $\sigma_w = 1$. No cutoff was employed and the wall potential was made to act *equally* on both particle species.

Monte Carlo simulations of this system were performed using a METROPOLIS algorithm within the grand canonical (μ, V, T) ensemble [25]. Three types of Monte Carlo moves were employed: (1) particle displacements, (2) particle insertions and deletions, (3) particle identity swaps: $1 \rightarrow 2$ or $2 \rightarrow 1$. To maintain the symmetry of the model, the chemical potentials μ_1 and μ_2 of the two components were set equal at all times. Thus only one free parameter, $\mu = \mu_1 = \mu_2$, couples to the overall number density $\rho = (N_1 + N_2)/V$. The other variables used to explore the wetting phase diagram were the reduced well depth $\epsilon/k_B T$ and the reduced wall potential $\epsilon_w/k_B T$. During the simulations, the observables monitored were the total particle density profile

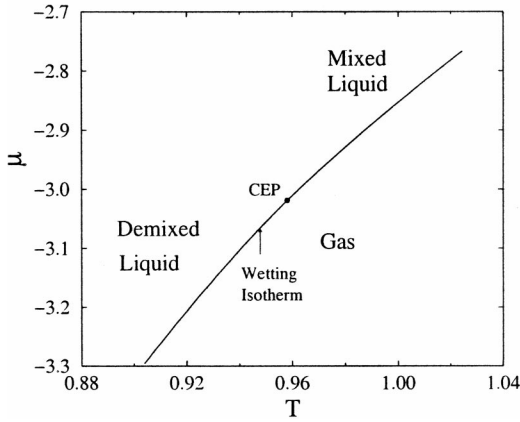


FIG. 9. The phase diagram in the μ - T plane (dimensionless units) of the symmetrical binary Lennard-Jones fluid model described in the text. Also shown is the location of the critical end point and the isotherm along which the wetting properties were studied.

$$\rho(z) = [N_1(z) + N_2(z)]/P^2, \quad (3.3)$$

the number difference order parameter profile,

$$n(z) = [N_1(z) - N_2(z)]/P^2. \quad (3.4)$$

These profiles were accumulated in the form of a histogram. Other observables monitored were the total interparticle energy and the wall interaction energy.

The choice of system size was, as ever, a compromise between minimizing finite-size effects and maximizing computational throughput. Tests showed the profiles to be largely insensitive to the size of the wall area and hence $p=7$ was used, this being the largest computationally tractable size consistent with the necessary choice of the slit width d . The latter must clearly be considerably larger than the film thicknesses of interest in order to prevent the liquid film directly interacting with the hard wall at $z=D$. In the results presented below, the typical slit width used was $d=16$, corresponding to some 40 molecular diameters. For thin films a narrower slit of width $d=8$ was used.

B. Wetting behavior along a subcritical isotherm

Accurate knowledge of bulk phase behavior is an essential prerequisite for detailed studies of near-coexistence wetting properties. In the present model, the locus of the liquid-vapor coexistence curve and location of the critical end point are already known to high precision from a previous Monte Carlo simulation study [9,5]. The phase diagram in the μ - T plane (in standard Lennard-Jones reduced units [25]) is shown in Fig. 9. The critical end point is located at $T_{\text{CEP}} = 0.958(3)$, $\mu_{\text{CEP}} = -3.017(3)$ [9,5]. We note that although the locus of the coexistence curve is known to five significant figures, the position of the CEP along this tightly determined line is known only to three significant figures.

To determine the wetting properties at temperatures below T_{CEP} the number density profile $\rho(z)$ was studied along the isotherm $T=0.9467$ as coexistence was approached from

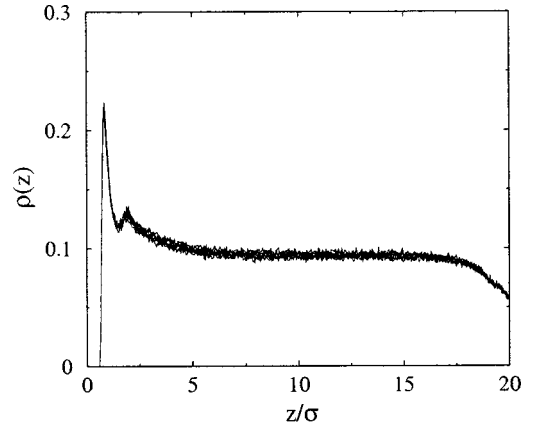


FIG. 10. Density profiles for $\epsilon_w = 1.0\epsilon$. Data are shown for seven values of $\mu - \mu_{cx}$ in the range $[0, -1.5]\epsilon$.

the vapor side. To achieve this, the chemical potential was incremented up to its coexistence value $\mu_{cx}(T)$ in a sequence of 6–10 steps of constant size $\Delta\mu = 0.0025$. This procedure was repeated for a number of different values of the wall-fluid potential strength ϵ_w , allowing the influence of this parameter on the wetting behavior to be ascertained. In all, six values of the ϵ_w were studied ($\epsilon_w = 1.0, 1.7, 1.75, 2.0, 3.0, 4.0$). We describe the wetting behavior for each in turn.

For $\epsilon_w = 1.0$, Fig. 10 shows that although the film thickness grows very slightly as coexistence is approached, it never exceeds two molecular diameters. At no point in the profile does the density attain that of the liquid phase ($\rho \approx 0.6$). The presence of a thin wetting layer right up to coexistence implies incomplete (partial) wetting.

Increasing the wall potential to $\epsilon_w = 1.70$ [Fig. 11], results in considerably more structure near the wall compared to $\epsilon_w = 1.0$, with clear density oscillations arising from excluded-volume “packing effects” [27]. The profile is much more responsive to changes in the chemical potential and reaches a thickness of 4–5 molecular diameters close to coexistence.

For $\epsilon_w = 1.75$, however, the situation changes qualitatively, as shown in Fig. 12. On increasing the chemical po-

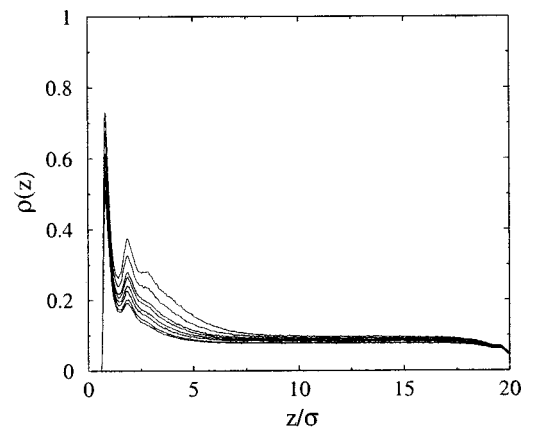


FIG. 11. Density profiles for $\epsilon_w = 1.7\epsilon$. Data are shown for eight values of $\mu - \mu_{cx}$ in the range $[0, -1.525]\epsilon$.

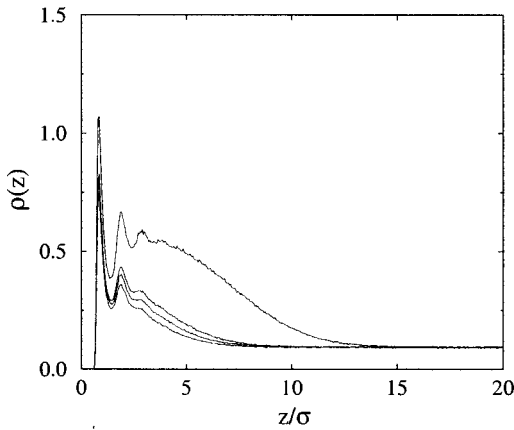


FIG. 12. Density profiles for $\epsilon_w = 1.75\epsilon$. Data are shown for six values of $\mu - \mu_{cx}$ in the range $[-0.025, -1.5]\epsilon$.

tential, a clear jump is observed in both the thickness of the film, and the value of its density. In the thick film, the density of a significant portion of the film is that of the bulk liquid. This thin-thick jump constitutes a prewetting transition, as previously observed in simulation studies of lattice gas models [26], Lennard-Jones fluids [13,14,27,28] as well as experimentally [29].

As the wall potential is increased to $\epsilon_w = 2.0$ (Fig. 13), the sharp prewetting transition is lost and instead the film thickness increases smoothly as μ approaches its coexistence value. This suggests that here the system is above the prewetting critical point [26].

On increasing ϵ_w to 3.0, a new feature emerges [Fig. 14(a)]. As the chemical potential increases, the thickness of the film initially increases smoothly with increasing μ . However, once the thickness reaches some 10 molecular diameters, a large jump occurs to a thickness of about 15 molecular diameters. Concomitant with this jump is a demixing of the film as a whole, as seen in the order-parameter profile Fig. 14(b). The size of the jump in the layer thickness appears to reduce as the wall strength is increased to $\epsilon_w = 4.0$ (Fig. 15), suggesting a weakening of the transition.

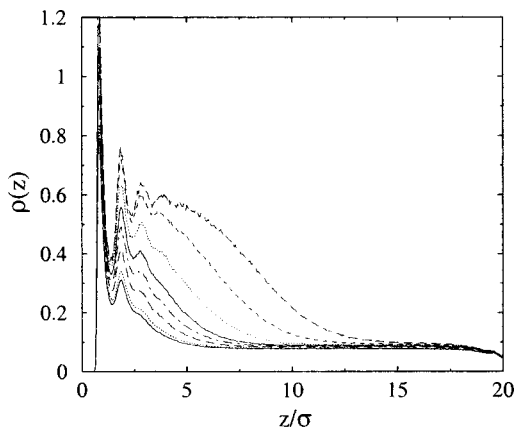


FIG. 13. Density profiles for $\epsilon_w = 2.0\epsilon$. Data are shown for eight values of $\mu - \mu_{cx}$ in the range $[-0.025, -1.6]\epsilon$.

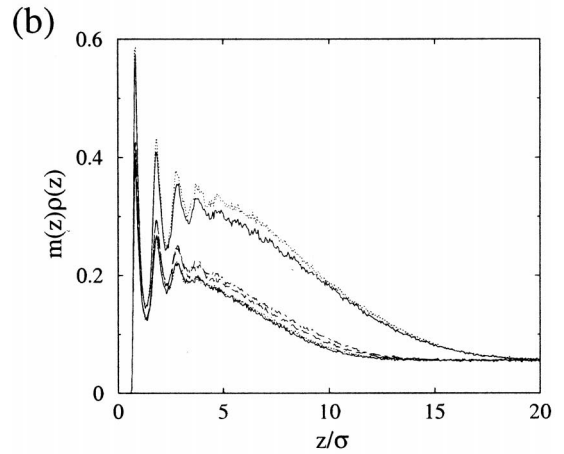
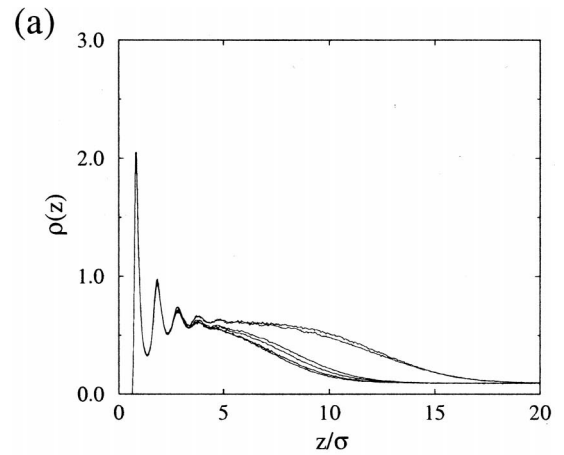


FIG. 14. (a) Density profiles for $\epsilon_w = 3.0\epsilon$. Data are shown for six values of $\mu - \mu_{cx}$ in the range $[-0.025, -1.55]\epsilon$, and (b) the corresponding order parameter profiles $n(z)$.

IV. DISCUSSION

The Monte Carlo simulation results at subcritical temperatures provide evidence that the mean-field calculations correctly identify the qualitative wetting behavior. They show that depending on the fluid-wall interaction strength ϵ_w , a number of different wetting scenarios occur as liquid-

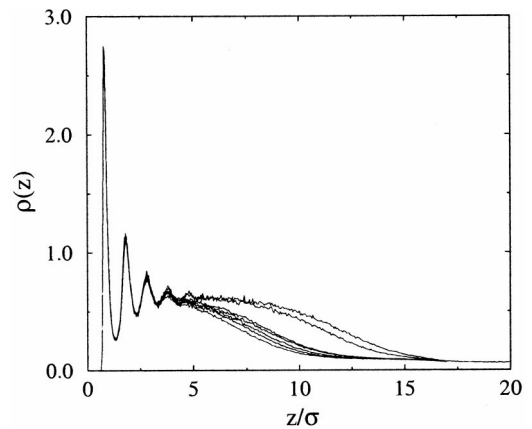


FIG. 15. Density profiles for $\epsilon_w = 4.0\epsilon$. Data are shown for eight values of $\mu - \mu_{cx}$ in the range $[-0.025, -1.6]\epsilon$.

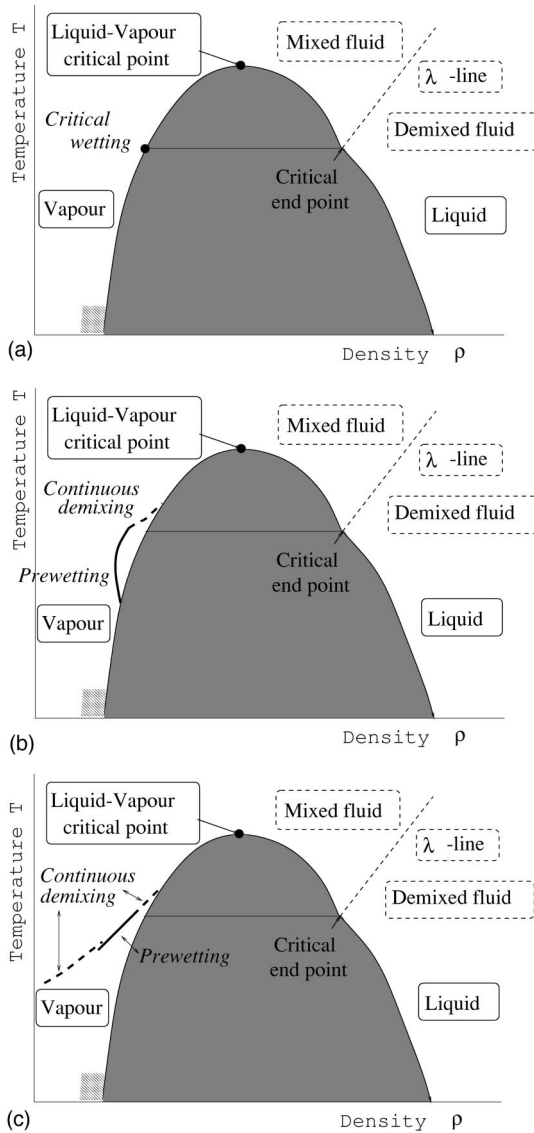


FIG. 16. Some possible schematic wetting phase diagrams in the temperature-density plane. (a) Weakly attractive wall: Critical end point T_{CEP} of the λ line is a critical wetting point, below which the wall is not wetted by the liquid. (b) Intermediate attraction: Demixing induced first order wetting transition at $T < T_{\text{CEP}}$ with a prewetting line that evolves into a second-order demixing line. (c) Strong attraction: Complete wetting at coexistence everywhere, but detached prewetting line or continuous demixing transitions off coexistence (in films of finite thickness). Hatched area indicates the possibility of conventional wetting transitions at lower temperatures.

vapor coexistence is approached from the vapor side. At small ϵ_w , only a very thin film builds up on the wall. For intermediate values of ϵ_w , a first prewetting transition is observed from a thin mixed film to a thick liquidlike mixed layer. Further increasing ϵ_w induces a second prewetting transition between a mixed liquidlike layer and a thicker demixed film, the situation being very similar to that shown in Fig. 6. The abrupt, first-order character of this latter transition appears to weaken on further increasing ϵ_w , in accord with the theoretical predictions.

We will now attempt to set our results within the context of the bulk phase diagram of the binary liquid. To this end, we discuss the possible wetting scenarios in the vicinity of the critical end point T_{CEP} . As previously argued in the Introduction, for temperatures $T < T_{\text{CEP}}$ sufficiently close to T_{CEP} the bulk correlation length ξ of the demixed liquid is larger than the thickness l_* of a mixed liquid layer at the wall. The state of order of the film thus depends strongly on the boundary conditions of the two interfaces confining the liquid layer. The nonselective liquid-vapor interface always favors mixing due to the reduced number of interacting neighbors in the interfacial region. The liquid-substrate interface, on the other hand, can either favor mixing or demixing depending on the strength of the fluid-wall potential. For a weakly attractive wall potential, mixing is favored because the particle density at the wall is low and the presence of the wall reduces the number of interacting neighbors. For a strongly attractive wall, however, the high density at the wall can counteract the missing neighbor effect leading to an overall demixing tendency.

If the net effect favors mixing at the wall, a continuous demixing of the layer as coexistence is approached can be excluded. A first-order transition involving a discontinuous increase of the film thickness upon demixing is still conceivable. However, we have shown in Sec. II A, that (at the mean-field level, at least) the demixed wetting film has a higher free energy than the corresponding mixed film provided the correlation length of composition fluctuations is sufficiently large.

At walls that suppress demixing, the film is thus always mixed close to the critical end point, and its thickness l_* below the critical end point is finite. Hence the critical end point is automatically a critical wetting point. The resulting phase diagram is shown schematically in Fig. 16(a). Note that the wetting transition here is pinned by a bulk phase transition, a situation somewhat reminiscent of triple-point wetting [30,11].

The situation changes if the substrate favors demixing. In this situation, one component segregates to the surface of the film already slightly above T_{CEP} and the order propagates continuously into the bulk of the film at T_{CEP} . The film remains wet at T_{CEP} . From the results of Sec. II C (in particular, Fig. 8), one can deduce two possible scenarios. The film may still exhibit a first-order wetting transition to a non-wet state at a temperature below T_{CEP} [(e.g., in Fig. 8) at $\phi_0 = 1.14$]. The discontinuous phase transition at liquid-vapor coexistence then spawns a prewetting line, which eventually switches into a second-order demixing line and loops around the critical end point as suggested in Fig. 16(b). If the wall is strongly attractive [(e.g., at $\phi_0 = 1.27$) in Fig. 8], the wall wets at all temperatures, the prewetting line detaches from the coexistence line and is continued by second-order demixing lines both at the high- and low-temperature side as sketched in Fig. 16(c).

ACKNOWLEDGMENTS

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